## PVT Lab Manual <br> Wanny Abdel Fattah Mohamed <br> The British University in Egypt


#### Abstract

Petroleum is a complex mixture of (sulfur, nitrogen, oxygen, helium) the physical and chemical properties of crude oils vary considerably and depend on the concentration of the various types of hydrocarbons and minor constituents present. And in the general there are there tests to measure hydrocarbon reservoir samples (Primary, Routine laboratory, Special laboratory PVT); Pouting laboratory test such as Compositional analysis of the system ,Constant-composition expansion ,Differential liberation ,Separator tests, and Constant-volume depletion.; Special laboratory PVT test such as Slim-tube test and Swelling test.


Index Terms : Fluid gravity, Specific gravity of the solution gas, Oil density, Gas solubility, Bubble-point pressure, Oil formation volume factor, Isothermal compressibility coefficient of under saturated crude oils, under saturated oil properties, Total formation volume factor, Crude oil viscosity, Surface tension.

## Introduction

Pressure-Volume-Temperature laboratory offers a comprehensive PVT program for all your reservoir fluid property requirements. Equipped with the latest equipment, PVT laboratory can provide a complete picture of any hydrocarbon sample. This data is essential for the economics and feasibility of any hydrocarbon reservoir. The experienced and specially trained staff can provide you accurate PVT analysis, which is vital for precisely calculating the reserves and also for evaluating the value of the reserve. Good PVT data ensures the reservoir is produced and managed in a controlled way, ultimately leading to maximum recovery. Such as

## -Black Oil PVT Analysis

Our PVT laboratory can analyze all types of black oil pressurized samples. Specific services offered include Pressure Volume Relationship's, Differential Vaporization experiments, Pressurized Viscosity determinations and Separator Test analysis.

## -Volatile Oil PVT Analysis

Volatile Oil PVT Analysis includes the analysis of volatile oil samples by means of the following techniques; Constant Composition Expansion measurement and Constant Volume Depletion analysis.
-Gas Condensate PVT Analysis
Pressure Volume Temperature laboratory analysis of gas condensate samples includes these services; Constant Composition Expansion measurement and Constant Volume Depletion analysis.

- Gas Compositional Analysis

Extended or basic gas compositional analysis utilizing modified gas chromatographs. Water Analysis

Standard oilfield water analysis utilizing wet chemistry and spectrometric analysis techniques

## Table of content:

|  | Page Number |
| :---: | :---: |
| Introduction | 1 |
| Preface | 4 |
| Sampling | 6 |
| Experiment No. 1: API Test | 10 |
| Experiment No. 2: FIuid Viscosity Test | 17 |
| Experiment No. 3 : Pour Point Test | 26 |
| Experiment No.4: Gas Formation Volume Factor Test | 28 |
| Experiment No. 5: Gas Density and Specific gravity Test | 30 |
| Experiment No. 6: Gas Viscosity Test | 32 |
| ExperimentN0.7: Classification of freervoir fuid Test | 36 |
| Experiment No. 8: Equilibrium Flash Separato Test | 42 |
| Experiment No. 9: Suffact ension Test | 45 |
| Experiment No.10: Geometers Test | 47 |
| Experiment So. 11: Gas Compressibility Test | 49 |
| Experiment No.12: Dalton's Law of Patial Pressures Test | 51 |
| Experiment No.13: Power of Hydrogen (PH) Test | 54 |
| Experiment No. 14: Acidity No | 57 |
| Experiment No.1: Emulsion Stability Test | 60 |
| Experiment No.16: Water Content Test | 62 |
| Appendix A: Conrersion Table | 64 |

## Preface

Petroleum is a complex mixture of (sulfur, nitrogen, oxygen, helium) the physical and chemical properties of crude oils vary considerably and depend on the concentration of the various types of hydrocarbons and minor constituents present. The properties of primary petroleum engineering include

* Fluid gravity
* Specific gravity of the solution gas
* Oil density
* Gas solubility
* Bubble-point pressure

4 Oil formation volume factor

* Isothermal compressibility coefficient of under saturated crude oils

4 Under saturated oil properties
4 Total formation volume factor
4 Crude oil viscosity

* Surface tension

And in the general there are there tests to measure hydrocarbon reservoir samples (Primary, Routine laboratory, Special laboratory PVT)

## 1. Primary test

Routines tests involving the measurements of the specific gravity and the gas-oil ratio of the produced Hydrocarbons fluids.
2. Routing laboratory test

These are several laboratory tests that are routinely

Compositional analysis of the system
ZConstant-composition expansion
Differential liberation
Separator tests
Constant-volume depletion
3. Special laboratory PVT test

Performed for very specific applications
Tests may be performed:
Slim-tube test
Swelling test


## Sampling

- The value to be attached to the laboratory determinations depends on whether the sample investigated is representative of the reservoir contents.
- The taking of samples can be accomplished either by subsurface sampling or by surface sampling.


## 1. Subsurface Sampling

- In this case a subsurface sampler is lowered into the well and kept opposite the producing layer for a sufficiently long time, figure in next slide.
- Subsurface samples can only be representative of the reservoir contents when the pressure at the point of sampling is above or equal to the saturation pressure. If this condition is not fulfilled, one should take a surface sample.



## 2. Surface Sampling

- In this case a subsurface sampler is lowered into the well and kept opposite the producing layer for a sufficiently long time, figure in next slide.
- Subsurface samples can only be representative of the reservoir contents when the pressure at the point of sampling is above or equal to the saturation pressure. If this condition is not fulfilled, one should take a surface sample.
- A sample of oil and gas is taken from the separator connected with the well (figures in next slides give sketches of vertical and horizontal separators and the arrangement for collecting different fluid samples).
- The surface oil and gas samples are recombined in the laboratory on the basis of the producing GOR.
in the field to obtain reliable samples and accurate measurement of the GOR and separator conditions. In the case of two or three stage separation the samples are taken from the high pressure separator.


Separator Liquid Sampling by Water Displacement

## Separator Gas Sampling



## EXPERIMENT NO. 1

## Fluid Density

## Theory

Separator Liquid Sampling by Gas
Displacement as the mass of a unit volume of the crude at a specified pressure and temperature. The specific gravity of a crude oil is defined as the ratio of the density of the oil to that of water. Both densities are measured at $60^{\circ} \mathrm{F}$ and atmospheric pressure; although the density and specific gravity are used extensively in the petroleum industry, the API gravity is the preferred gravity scale. This gravity scale is precisely related to the specific gravity.

The American Petroleum Institute gravity, or API gravity, is a measure of how heavy or light petroleum liquid is compared to water. If its API gravity is greater than 10 , it is lighter and floats on water; if less than 10 , it is heavier and sinks. API gravity is thus an inverse measure of the relative density of a petroleum liquid and the density of water, but it is used to compare the relative densities of petroleum liquids. For example, if one petroleum liquid floats on another and is therefore less dense, it has a greater API gravity. Although mathematically, API gravity has no units (see the formula below), it is nevertheless referred to as being in "degrees". API gravity is gradated in degrees on a hydrometer instrument. The API scale was designed so that


Figure 1.1: Typical Pycnometer
Figure 1.2: Typical Hydrometer

The Pycnometer as shown below is used to determine density of reservoir fluid which consists of a constant volume cup with a cover which contains hole in the middel
The as shown below is used to determine density of reservoir fluid which consists of a constant volume cup with a cover which contains hole in the middel .


Figure 1.3: Typical U-Tube

At the same level the pressure extracted by the the oil column is equal to the pressure extracted by the water column so:
$\mathrm{Po}=\mathrm{Pw}$
Gravity*Density $_{w} *$ height $_{w}=$
Gravity*Densityo *height ${ }_{0}$
Density $_{\mathrm{w}}{ }^{*}$ height $_{\mathrm{w}}=$
Densityo ${ }^{*}$ height $_{\text {}}$
Height $_{\mathrm{w}} /$ height $_{0}=$ Density ${ }$
Density $_{w}$
Height $_{\text {w }} /$ height $_{\mathrm{o}}=$ Sp.gr

$$
\text { API gravity }=\frac{141.5}{\mathrm{hw} / \mathrm{ho}}-131.5
$$

## Measurement of API gravity from its density

To derive the API gravity from the density, the density is first measured using either the hydrometer, detailed in ASTM D1298 or with the oscillating Utube method detailed in ASTM D4052. Density adjustments at different temperatures, corrections for soda-lime glass expansion and contraction and meniscus corrections for opaque oils are detailed in the Petroleum Measurement Tables, details of usage specified in ASTM D1250. The specific gravity is then calculated from the formula below and the API gravity calculated from the first formula above.

$$
\mathrm{SG} \text { oil }=\frac{\rho_{\mathrm{oil}}}{\rho_{\mathrm{H}_{2} \mathrm{O}}}
$$

## Classifications or grades

Generally speaking, oil with an API gravity between 40 and 45 commands the highest prices. Above 45 degrees the molecular chains become shorter and less valuable to refineries.

Efitaze.5ilf is classified as light, medium or heavy, according to its measured API gravity.

- Light crude oil is defined as having an API gravity higher than 31.1 ${ }^{\circ}$ API (less than $870 \mathrm{~kg} / \mathrm{m}^{3}$ )
- Medium oil is defined as having an API gravity between $22.3^{\circ} \mathrm{API}$ and $31.1^{\circ} \mathrm{API}$ ( 870 to $920 \mathrm{~kg} / \mathrm{m}^{3}$ )
- Heavy crude oil is defined as having an API gravity below $22.3^{\circ} \mathrm{API}$ ( 920 to $1000 \mathrm{~kg} / \mathrm{m}^{3}$ )
- Extra heavy oil is defined with API gravity below $10.0^{\circ} \mathrm{API}$ (greater than $1000 \mathrm{~kg} / \mathrm{m}^{3}$ )

Not all parties use the same grading.
The United States Geological Survey uses slightly different definitions.

Crude oil with API gravity less than 10 ${ }^{\circ} \mathrm{API}$ is referred to as extra heavy oil or bitumen. Bitumen derived from the oil sands deposits in the Alberta, Canada area has an API gravity of around 8 ${ }^{\circ}$ API. It is "upgraded" to an API gravity of $31^{\circ}$ API to $33^{\circ} \mathrm{API}$, and the upgraded oil is known as synthetic crude.

## Calibration

1. Remove the lid from the cup, and ${ }^{1931}$ completely fill the device with water after heating it till reach $60^{\circ} \mathrm{F}$ (make sure the thermometer)
2. Replace the lid and wipe dry.
3. Use the balance in order to get the net weight of the water.
4. Calculate the density by dividing the net weighton the volume which is writen on the device.

## API gravity formulas

The formula to obtain API gravity of petroleum liquids, from specific gravity (SG), is:

$$
\text { API gravity }=\frac{141.5}{\mathrm{SG}}-131.5
$$

${ }^{\text {ISSN }}$ 2zoinilvirsely, the specific gravity of
petroleum liquids can be derived
from the API gravity value as

$$
\text { SG at } 60^{\circ} \mathrm{F}=\frac{141.5}{\text { API gravity }+131.5}
$$

Thus, a heavy oil with a specific gravity of 1.0 (i.e., with the same
Results: density as pure water at $60^{\circ} \mathrm{F}$ ) would have an API gravity of:

$$
\frac{141.5}{1.0}-131.5=10.0^{\circ} \mathrm{API}
$$

## Procedure:

$$
\mathrm{API}=\frac{141.5}{\gamma}-131.5
$$

## RESULTS OF DENSITY TEST

## Room

Temp........... ${ }^{\circ} \mathrm{F}$
Fluid
Temp........... ${ }^{\circ} \mathrm{F}$

1. We pick up a pycnometer and wash it very carefully by dry air until we are completely sure that its clean and dry
2. weight the Bycnometer empty
3. Make sure that the pycnometer is completely filled until the specific label
4. But volatile oil in it
5. Wight the pycnometer full of volatile
6. Calculate the net weight of the desired fluid by subtracting the empty weight of pycnometer from filled weight of pycnometer
7. But heavy oil in the Bycnometer
8. Wight the heavy oil that in Bycnometer
9. Do these steps for the condensate
10. And do it by using water
11. Calculate the weight of (condensate and volatile oil and the heavy oil )

|  |  | WT of |  |  |  |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :--- |
| Pycnometer <br> volume(ml) | WT of <br> Pycnometer <br> empty(gm) | Pycnometer <br> filled with <br> fluid (gm) | net <br> weight <br> (gm) | Density <br> gm/ml | sp-gr | API | fluid type |
| :--- |

## Comments:

$\qquad$
$\qquad$

## Errors:

## Error analyses:

## EXPERIMENT NO. 2

## Fluid Viscosity

## Aim:

The aim of this experiment is to calculate the viscosity of a certain oil sample. Viscosity helps a
time-measuring, instrument that operates on the principle of the measurement of time required for a rolling ball, affected by shear and pressure of the fluid, to travel a pre-determined distance at controlled conditions. It employs a rolling steel ball for determining the dynamic viscosity of liquid-phase samples at constant temperatures and pressures. The ball is positioned inside the measuring barrel with the test fluid sample so that it is limited to only rolling type motion. An electronic timer records the time required for the ball to roll through the barrel.

The Chandler high pressure Rolling Ball Viscometer is a precision instrument used to determine the viscosity of bottom-hole and surface samples of reservoir oils at elevated temperatures and pressures to $10,000 \mathrm{psi}$ at $300^{\circ} \mathrm{F}$. Accurate and reproducible engineering data is obtainable, whether the specific application is to determine the viscosity of petroleum
fluids at simulated reservoir conditions, or liquid phase viscosities at other predetermined pressures and temperatures. The samples measured must be electrically non-conductive. The viscometer operates on a rolling-ball principle where the roll-time of a $1 / 4$-inchdiameter ball is used to obtain viscosity data. Viscosity values are then obtained by correlation of the measured data with curves of fluids with known viscosities and densities.

## Safety Requirements

- Operator SHOULD avoid contact with the bare surface of the test assembly jacket when in operation. The instrument control box SHOULD NOT at any time be opened during operation. An
unskilled person SHOULD NOT troubleshoot potentially dangerous equipment. Safety SHOULD NOT be assumed. The operator must keep in mind, even the most sophisticated instrument cannot think; (a) insulators do not always insulate, (b) conductors do not always conduct properly, (c) resistors do not always dissipate the required heat. For these reasons, the operator should carefully follow the outlined instructions of this manual and consult the manufacturer when specific questions arise. CAUTION: Exposure to $\mathrm{H}_{2} \mathrm{~S}$ is potentially fatal. Use adequate safety procedures when handling $H_{2}$ S samples. Consult your safety department for proper procedures for handling $\mathrm{H}_{2} \mathrm{~S}$.


## Operation

In the rolling-ball viscometer, the time it takes a metal ball to roll from one end of a fluid filled tube to the other is an indication of the viscosity for the fluid. Mathematically this is expressed as

In the rolling-ball viscometer, the time it takes a metal ball to roll from one end of a fluidfilled tube to the other is an indication of the viscosity for the fluid. Mathematically this is expressed as:

$$
\mu=\frac{\left(\rho_{B}-\rho_{F}\right) g R^{2} \sin \theta}{v_{\infty}}
$$

Where,

| $\mu$ | $=$ | Dynamic Viscosity |
| :--- | :--- | :--- |
| $\rho_{B}$ | $=$ | Density of the ball |
| $\rho_{F}$ | $=$ | Density of the fluid |
| $g$ | $=$ | Acceleration due to gravity |
| $R$ | $=$ | Diameter of the ball |
| $\theta$ | $=$ | Angle of the measuring barrel |
| $v_{\infty}$ | $=$ | Velocity normal to the Earth in the down direction |
|  |  | Defined as distance over time $(d / t)$ |

For a given set of tests, the distance variable of the velocity term, along with $g, R$ and $\theta$, remain constant. Therefore, the above equation can be conveniently expressed as follows:

$$
\mu=K t\left(\rho_{B}-\rho_{F}\right)
$$

From the above equation it can be seen that for a constant ball and fluid density ( $\rho_{B-}-\rho_{F}$ ), the viscosity $(\mu)$ is directly proportional to the ball roll-time ( $t$ ). Effectively, the ball is forced down the tube due to gravitational effects at a rate dependent upon the fluid viscosity and the difference between the density of the ball and that of the fluid. Any increase in fluid density reduces the effect of gravity acting on the ball. The ball will correspondingly fall more slowly (an increase of the $t$ term), and indicates a higher viscosity value. Conversely, as the density term diminishes to zero, the viscosity value also approaches zero.

1. Choose the correct ball size. This can be done by examining the sample fluid. If the fluid viscosity is estimated to be below 25 centipoise (above $25^{\circ} \mathrm{API}$ ), a .252 - or .248inch diameter ball should be used. Above 25 centipoise (below $25^{\circ} \mathrm{API}$ ), the .234 -inch diameter ball will be appropriate. The balls are not interchangeable and must be kept separate.
2. Clean the test assembly. Since the barrel, ball and inner chamber must be completely free of dirt and lint, care should be taken to secure a clean test assembly before
undertaking any measurements. Light oil, such as kerosene, and thin paper should be used to clean the ball and chamber.
3. Place the ball in the bottom of the empty measuring barrel from the upper end of the assembled test unit.
4. Evacuate the test assembly. This is done by opening the vacuum pump valve at the lower end of the unit and closing the charging valve. 5. Charge the test sample fluid to the viscometer. The vacuum valve should be closed while the high pressure charging valve should now be reopened.
5. Rock the test assembly to obtain a single-phase sample. A mixing device called the "Slip
Ring Mixer" is installed to facilitate the effort. Effectively, the task is completed when pressure fluctuations of the sample have ended.
Sufficient time afterwards should be allowed to permit the newly liberated gas bubbles to escape from the measuring barrel.
Particularly in the case of heavy fluids, a bubble trapped under the ball will sometimes
hinder it from free-fall. The surface tension of the oil prevents the bubble from passing
 bubble thus reduces the weight of the ball and lengthens its roll-time or might prevent electrical contact entirely.
6. Set the temperature of the viscometer to the desired test temperature with the barrel valve open. First, the main power switch (Item \#10) must be switched to the $\mathbf{O N}$ position. Set the desired temperature on the temperature controller (Item \#9; this is done by pressing the UP and DOWN arrows; refer to manufacturers' manual for instructions). The OP 1
light will illuminate to indicate the proper temperature cycling. During heating, it is very important that the chamber be open to a pressure control system. Allow one hour after the temperature set point has been reached for the test unit and sample to reach thermal equilibrium. Once the desired temperature and pressure has stabilized, rock the test assembly again to homogenize the sample and then close the charging valve.
with the barrel valve plunger (Item \#1 from Drawing \#1602-1). At this time, the appropriate resolution of the timer may be determined. The Timer has a 6-digit display with a maximum resolution of 0.001 seconds; this setting yields a maximum test time of approximately 16 minutes and 40 seconds. If the ball takes longer than this to fall from the bottom to the top, adjust the resolution of the Timer (refer to manufacturers' manual for instructions).
7. Energize the solenoid with the Coil toggle switch (Item \#11) in the ON position. Now the ball can be held in the TOP position. The test unit is then returned to the operating position.
8. Zero the clock by pushing the RST button on the Timer (Item \#7).
9. Release the ball by pressing the DROP button. The TIMER will start when the ball is no longer in contact with the barrel valve plunger. When the ball makes contact at the end of the roll, the Timer stops, the Alarm (Item \#5) sounds and the Bottom light illuminates.
10. Bring the ball into the TOP position at the upper end of the measuring barrel by rotating the receptacle arm handle (Item \#49; See Drawing \#1602-1). The handle should be rotated towards the upper end of the test unit until the $180^{\circ}$ stop assembly (Item \#67) engages with the stop lug mounted on the test unit. The Top indicator (Item \#6) will illuminate when the ball has travelled through the length of the barrel and made contact

## Calibration

As stated previously, operation of the Chandler Rolling Ball Viscometer is based on the following equation:

## Where,

\mu}==\mathrm{ Dynamic Viscosity
\mu}==\mathrm{ Dynamic Viscosity
K}=\mathrm{ Calibration Constant
K}=\mathrm{ Calibration Constant
t = Roll Time
t = Roll Time
\rho}=\quad= Density of the Ball
\rho}=\quad= Density of the Ball
\rhoF
\rhoF

# Figure 1.4: Rrolling 

The Calibration Constant ( $K$ ) is dependent upon the size of the ball, the angle of the measuring barrel and the vertical distance traveled. Therefore, everything else being equal, the value of $K$ varies with each ball and roll angle. A calibration should be conducted for each individual ball used at each measuring angle.
Chandler Engineering recommends an annual "spot check" of the Calibration Constant for each ball used, at each angle and at least three (3) temperatures. A simple "spot check" procedure would be to measure the viscosity of a Viscosity Standard. A full calibration should also be performed if any critical component (the ball, measuring barrel, coil assembly, lower contact assembly, control cable or control box) is replaced.

## Ball Viscometer

## Calibration Procedure

One or more Viscosity Standards (fluids of known density and viscosity at test temperatures) should be used. A roll-time mean is taken from five consistent readings at each desired Roll Angle. All calibrating tests are made at atmospheric pressure.

1. Choose the correct ball size. If the viscosity of the Viscosity Standard is below 25 centipoise (above $25^{\circ} \mathrm{API}$ ), a .252- or . 248 -inch diameter ball should be used. Above 25 centipoise (below $25^{\circ} \mathrm{API}$ ), the .234 -inch diameter ball will be appropriate. The balls are not interchangeable and must be kept separate.
2. Check the diameter and density of the selected ball.
3. Select a minimum of three (3) Test

Temperatures from the data sheet of the Viscosity Standard. Typically these are:
a. Ambient $\left(77^{\circ} \mathrm{F}\right.$ or $\left.25^{\circ} \mathrm{C}\right)$
b. Mid-Range $\left(122^{\circ} \mathrm{F}\right.$ or $\left.50^{\circ} \mathrm{C}\right)$
c. High Temperature $\left(212^{\circ} \mathrm{F}\right.$ or $\left.100^{\circ} \mathrm{C}\right)$

WARNING: Select temperatures that are
BELOW the Boiling Point of the Viscosity Standard.
4. Clean the test assembly. Since the barrel, ball and inner chamber must be completely
free of dirt and lint, care should be taken to secure a clean test assembly before
undertaking any measurements. Light oil, such as kerosene, and thin paper should be used to clean the ball and chamber.
5. Place the ball into the empty measuring barrel while in a horizontal position. Slowly raise
 gently roll to the bottom.
6. Fill the viscometer with the Viscosity Standard.

Rock the test assembly to obtain a single-phase sample.
7. Set the temperature controller to the first test temperature. Allow one hour after the set point has been reached to allow the temperature to balance throughout the unit.
8. Run several roll tests until at least five (5) consistent roll times are obtained at each measuring angle: $70^{\circ}, 45^{\circ}$, and $23^{\circ}$.
9. Repeat steps 7 and 8 above for each test temperature.
10. Select as many different Viscosity Standards 1938 as required and repeat the above procedure.
11. Compute the mean roll time for each set of roll times (i.e. for each combination of ball, measuring angle, Viscosity Standard and temperature).
12. Divide the known viscosity of the Viscosity Standard by the product of the mean roll time and the difference in density of the selected ball and that of the Viscosity Standard.
This is the Calibration Constant. Tables similar to the one below may facilitate this process.

| Test Temperature | ${ }^{\circ} \mathrm{F}$ |  |
| :--- | :--- | :--- |
| Roll Angle | $23^{\circ} \quad 45^{\circ} \quad 70^{\circ}$ |  |
| Density of Ball $\left(\rho_{B}\right)$ | $\mathrm{g} / \mathrm{cc}$ |  |
| Density of Fluid $\left(\rho_{F}\right)$ | $\mathrm{g} / \mathrm{cc}$ |  |
| $\Delta \rho\left(\rho_{B}-\rho_{F}\right)$ | $\mathrm{g} / \mathrm{cc}$ |  |
| Viscosity of Standard at Temperature $(\mu)$ | cP |  |
| Roll Time | $\mathbf{1}$ | s |
| 2 | s |  |
| $\mathbf{3}$ | s |  |
| $\mathbf{4}$ | s |  |
| $\mathbf{5}$ | s |  |
| Mean Roll Time $(t)$ | s |  |
| Calibration Constant $\mathrm{K}=\mu /(t \Delta \rho)$ |  |  |


| Calibration Fluid |  |  |  |
| :---: | :---: | :---: | :---: |
| Test Temperature | $77.00{ }^{\circ} \mathrm{F}$ | $122.00{ }^{\circ} \mathrm{F}$ | $212.00 \quad{ }^{\circ} \mathrm{F}$ |
| Fluid Density ( $\rho_{\mathrm{F}}$ ) | $0.8731 \mathrm{~g} / \mathrm{mL}$ | $0.8575 \mathrm{~g} / \mathrm{mL}$ | $0.8262 \mathrm{~g} / \mathrm{mL}$ |
| $\Delta \rho\left(\rho_{\mathrm{B}}-\rho_{\mathrm{F}}\right)$ | $6.8978 \mathrm{~g} / \mathrm{mL}$ | $6.9134 \mathrm{~g} / \mathrm{mL}$ | $6.9447 \mathrm{~g} / \mathrm{mL}$ |
| Known Viscosity ( $\mu_{C}$ ) | 104.1 cP | 29.77 cP | 6.227 cP |
| Mean Roll Time ( $t$ ) | 4.909 s | 1.401 | 0.292 s |
| $\begin{gathered} \text { Calibration Constant }(K) \\ K=\mu_{C} /(t \Delta \rho) \end{gathered}$ | 3.0743 | 3.0736 | 3.0707 |

This example viscosity measurement was then performed using the test fluid at the same test conditions of the calibration ( 0.252 ball, $70^{\circ}$ barrel angle, atmospheric pressure). The density of the
test fluid at test temperatures was measured or obtained prior to the test. Again, several roll tests were conducted at each test temperature until consistent results were obtained.

## VISCOSITY MEASURMENT

| Test Fluid |  |  |  |  |  |  |  |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: | :---: |
| Test Temperature | 77.00 | ${ }^{\circ} \mathbf{F}$ | 122.00 | ${ }^{\circ} \mathbf{F}$ | 212.00 | ${ }^{\circ} \mathbf{F}$ |  |
| Fluid Density $\left(\rho_{\mathrm{F}}\right)$ | 0.8728 | $\mathrm{~g} / \mathrm{mL}$ | 0.8559 | $\mathbf{g} / \mathbf{m L}$ | 0.8219 | $\mathrm{~g} / \mathrm{mL}$ |  |
| $\Delta \rho\left(\rho_{\mathrm{B}}-\rho_{\mathrm{F}}\right)$ | 6.8981 | $\mathrm{~g} / \mathrm{mL}$ | 6.9150 | $\mathbf{g} / \mathbf{m L}$ | 6.9490 | $\mathrm{~g} / \mathbf{m L}$ |  |
| Mean Roll Time $(t)$ | 0.371 | s | 0.177 | s | 0.068 | s |  |
| Measured Viscosity $\left(\mu_{M}\right)$ <br> $\mu_{\boldsymbol{M}}=\boldsymbol{K} t \Delta \rho$ | 7.868 | $\mathbf{c P}$ | 3.762 | $\mathbf{c P}$ | 1.451 | $\mathbf{c P}$ |  |

2- Digital balance.


Equipment:
1- Oil sample

3- Rolling ball viscometer


4- Pycnometer


## Procedures:

1- Put the sample in the rolling ball viscometer

2- Hold the ball
3- Drop the ball and switch on the device at the same time.

4- The rolling ball viscometer at angle $=70$

5- Weigh the pycnometer
6- Weight the pycnometer filled with oil
7- Determine the weight of the oil sample.

## Results:

$$
\mu=\frac{\left[(\rho \mathbf{b}-\rho \mathbf{f}) \mathbf{g ~ R}{ }^{2} \sin \bar{Z}\right]}{\mathbf{v}}
$$

V is the velocity of the ball $(\mathrm{v}=\mathrm{d} / \mathrm{t})$
Distance over the time
K is calibration constant $\rightarrow \mathrm{K}=\frac{\mathrm{gR}^{2} \boldsymbol{\operatorname { s i n }}^{2}-}{\mathrm{d}}$
$\rho f=\quad \mathrm{gm} . / \mathrm{cc}$
$\mathrm{t}=\quad \mathrm{sec}$
$\mathrm{k}=\quad(\mathrm{cm} / \mathrm{sec})^{\wedge} 2$

Condition of caliberation ( 0.252 inch ball diameter 70 parrel angle, atmospheric preesure )
the density of the test fluid
Test temp $=122 \mathrm{~F}$
Density of fluid=
Time $=\mathrm{sec}$
(density $\rho_{B}=7.7709 \mathrm{~g} / \mathrm{cc}$ ), the Measuring Barrel at and angle of $70^{\circ}$ (use thermometer to make sure the fluid`s tempertue is 122 F foe density \& viscosity) and at atmospheric pressure

Comments:
.........................................................................
$\qquad$

The Pour Point test for crude oil is

## Error analyses:

 designed to identify difficulties in storage and handling of crude oil with unusually high oil pour point. (Never store fuel near or below the tested oil pour point) where by the Pour Point is the lowest temperature at which fuel can be handled before the viscosity becomes unmanageable even for positive displacement fuel transfer pumps. Fuel is easy to keep warm but once "set" in this way it can be very difficult to re-liquefy with obvious consequences; this really is a very simple test with instructions and equipment provided in the Lab
## Error analyses:

## Test Procedure

1- Fetch the oil sample and put it by angle 45 degree.
2- Use water path or oven to begin heating the sample.
3- Insert thermometer into crude to measure the temperature.
4- Observe the sample until the first drop appears.
5- Record the temperature at this point.

## EXPERIMENT NO. 4

## GAS FORMATION VOLUME FACTOR

 Theory

## Comments:

$\qquad$

## Errors:

$\qquad$
$\mathrm{T}=$ temperature, ${ }^{\circ} \mathrm{R}$
In other field units, the gas formation volume factor can be expressed in $\mathrm{bbl} / \mathrm{scf}$, to give: $\quad \mathrm{Bg}=0.005035$ ZT/P

The reciprocal of the gas formation volume factor is called the gas expansion factor and is designated by the symbol Eg , or

$$
\mathrm{Eg}=35.37 \mathrm{P} / \mathrm{ZT}
$$

$\mathrm{scf} / \mathrm{ft}^{3}, \mathrm{Eg}=198.6 \mathrm{P} / \mathrm{ZT}$ scf/bbl

## Test Procedure

1. Starting by Gas sample at 60 F \& 14.7 psia.
2. Use the oven to heat the sample until reach certain temperature.
3. Use Jog mode then increase the volume of the Gas sample.
4. Record the new Temperature \& Pressure.
5. Calculate Z factor

$$
\mathrm{z}=\frac{\mathrm{V}_{\mathrm{R}} p_{\mathrm{R}} \mathrm{~T}_{\mathrm{se}}}{\mathrm{~V}_{\mathrm{sc} P \mathrm{sc}} \mathrm{~T}_{\mathrm{R}}}
$$

6. Calculate Bg use the above formula.

## Results

$\qquad$

## Comments:

$\qquad$
$\qquad$
$\square$

## Errors:

$\qquad$

## Error analyses:

$\qquad$

## EXPERIMENT NO. 5

## Gas Density \& Specific Gravity

## Theory

One of the main gas properties that are frequently of interest to engineers is the apparent molecular weight. If yi represents the mole fraction of the component in a gas mixture, the apparent molecular weight is defined mathematically by the following equation:
$\mathrm{M}_{\mathrm{a}}=\sum \mathrm{yi} \mathrm{Mi}$

Where $\mathrm{Ma}=$ apparent molecular weight of a gas mixture
$\mathrm{Mi}=$ molecular weight of the component in the mixture $y i=$ mole fraction of component $i$ in the mixture
The density of an ideal gas mixture is calculated by simply replacing the molecular weight of the pure
component with the apparent molecular ${ }^{1944}$ weight of the gas mixture to give:

$$
\rho_{\mathrm{g}}=\mathrm{PMa} / \mathrm{RT}=\mathrm{m} / \mathrm{V}
$$

Where $\rho_{\mathrm{g}}=$ density of the gas mixture, lb/ft3

$$
\begin{aligned}
\mathrm{P} & =\mathrm{psia} \\
\mathrm{~T} & =\mathrm{R}
\end{aligned}
$$

The specific gravity is defined as the ratio of the gas density to that of the air. Both densities are measured or expressed at the same pressure and temperature. Commonly, the standard pressure $\mathrm{p}_{\mathrm{sc}}$ and standard temperature $\mathrm{T}_{\mathrm{sc}}$ are used in defining the gas specific gravity:

$$
\gamma=\rho_{\mathrm{g}} / \rho_{\mathrm{air}}=\mathrm{Ma} / \mathrm{M}_{\mathrm{air}}
$$

where $\gamma \mathrm{g}=$ gas specific gravity
$\rho_{\text {air }}=$ density of the air
$\mathrm{M}_{\text {air }}=$ apparent molecular weight of the air $=28.96$

## Test Procedure

1. Starting by Gas sample at 60 F \& 14.7 psia.
2. Use Jog mode then increase the volume of the Gas sample.
3. Record the new Temperature, Pressure, and Volume.
4. Calculate Z factor
5. Use $\mathbf{G C}$ to obtain mole friction.
6. Calculate Gas gravity \& density use the above formulas.

$$
\rho_{\mathrm{g}}={ }^{=} 300 * 16.5617924 / 10.7 / 630=0.74 \mathrm{lb} / \mathrm{ccu} . \mathrm{ft}
$$

$$
\gamma=\rho_{\mathrm{g}} / \rho_{\mathrm{air}}=\mathrm{Ma} / \mathrm{M}_{\mathrm{air}}
$$

## Results

## Comments:

## Errors:

Tffeezairf- Kobayashi-Burrows Correlation Method
Carr, Kobayashi, and Burrows (1954) developed graphical correlations for estimating the viscosity of natural gas as a function of temperature, pressure, and gas gravity. The computational procedure of applying the proposed correlations is summarized in the following steps:

Step 1. Calculate the pseudo-critical pressure, pseudo-critical temperature, and apparent molecular weight from the specific gravity or the composition of the natural gas. Corrections to these pseudocritical properties for the presence of the nonhydrocarbon gases (CO2, N2, and H2S) should be made if they are present in concentrations greater than 5 mole percent.
Step 2. Obtain the viscosity of the natural gas at one atmosphere and the temperature of interest from Figure 2-5. This viscosity, as denoted by $\mu 1$, must be corrected for the presence of nonhydrocarbon components by using the inserts of Figure 2-5. The nonhydrocarbon fractions tend to increase the viscosity of the gas phase. The effect of nonhydrocarbon components on the viscosity of the natural gas can be expressed
mathematically by the following relationships:

$$
\begin{aligned}
& \mu_{1}=(\mu 1) \text { uncorrected }+(\Delta \mu)_{\mathrm{N} 2} \\
& +(\Delta \mu)_{\mathrm{CO} 2}+(\Delta \mu)_{\mathrm{H} 2 \mathrm{~S}}
\end{aligned}
$$

where $\mu_{1}=$ "corrected" gas viscosity at one atmospheric pressure and reservoir temperature, cp
$(\Delta \mu)_{\mathrm{N} 2}=$ viscosity corrections due to the presence of N 2
$(\Delta \mu)_{\mathrm{CO} 2}=$ viscosity corrections due to the presence of CO 2
$(\Delta \mu)_{\mathrm{H} 2 \mathrm{~S}}=$ viscosity corrections due to the presence of H 2 S
$\left(\mu_{1}\right)$ uncorrected $=$ uncorrected gas viscosity, cp
Step 3. Calculate the pseudo-reduced pressure and temperature.
Step 4. From the pseudo-reduced temperature and pressure, obtain the viscosity ratio $\left(\mu_{\mathrm{g}} / \mu_{1}\right)$ from Figure 2-6. The term $\mu \mathrm{g}$ represents the viscosity of the gas at the required conditions.
Step 5. The gas viscosity, $\mu_{\mathrm{g}}$, at the pressure and temperature of interest is calculated by multiplying the viscosity at one atmosphere and system temperature, $\mu 1$, by the viscosity ratio.

## The following examples illustrate the

 use of the proposed raphical correlations:$$
\left.\left.\begin{array}{rl}
\mu_{\mathrm{s}}= & \frac{\sum}{\sum_{j} \mu_{\mathrm{s}} \mathrm{y}_{\mathrm{j}} \mathrm{M}_{\mathrm{j}} \mathrm{M}_{\mathrm{j}}^{1 / 2}} \\
\mu_{1}=\left(\mu_{1}\right)_{\mathrm{uncorrected}}+(\Delta \mu)_{\mathrm{N}_{2}}+(\Delta \mu)_{\mathrm{CO}_{2}}+(\Delta \mu)_{\mathrm{H}_{2} \mathrm{~S}}
\end{array}\right] \begin{array}{rl}
\text { where } \quad \mu_{1} & =\text { "corrected" gas viscosity at one atmospheric } \\
& \text { pressure and reservoir temperature, cp }
\end{array}\right\} \begin{aligned}
(\Delta \mu)_{\mathrm{N}_{2}} & =\text { viscosity corrections due to the presence of } \mathrm{N}_{2} \\
(\Delta \mu)_{\mathrm{CO}_{2}} & =\text { viscosity corrections due to the presence of } \mathrm{CO}_{2} \\
(\Delta \mu)_{\mathrm{H}_{2} \mathrm{~S}} & =\text { viscosity corrections due to the presence of } \mathrm{H}_{2} \mathrm{~S}
\end{aligned}
$$



Reservoir Engineering Handbook

Figure 2-5. Carr's almospheric gas viscosity correlation. (Permission to publish by the Society of Perroleum Engineers of AlME. Copyright SPE-AMME.)

SRN
170 F
$=0.0093 * 1.1=0.01023$ C.P

| Component | Mole \% | Yi | Mi | yiMi | Tci R | Pci <br> psia | yiTci | yiPci |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
| Total |  | 0.99947 |  |  |  |  |  |  |

$\begin{array}{llll}\text { Sp.gr C7+= } & \text { Tr } & & \text { Pr } \\ & \mathrm{T}=\quad \mathrm{F} & \mathrm{P}=\quad \text { Psia }\end{array}$

## Error analyses:

## Comments:

## Errors:

$\qquad$

- the position of its critical point.


## Importance of determination fluid type

The following reasons determine the importance of knowing fluid type it determines:

## EXPERIMENT NO. 7

## Classification of Reservoir Fluids

 Five Reservoir FluidsThe petroleum engineer should determine the type of fluid very early in the life of his reservoir ;
the behavior of a reservoir fluid during production is determined by

- the shape of its phase diagram where by The shapes of the phase diagrams can be used in understanding the behavior of multicomponent mixtures



10. Repeat the same procedure until the $1^{\text {st }}$ bubble appears.
11. Increase the temperature a little bit afterward repeat the same procedure until get the rest of $1^{\text {st }}$ bubbles point's pressure.
12. Connect between the bubbles point's pressures for drawing bubble point line.
13. Starting by live crude sample at low temperature \& high pressure then decrease the pressure by constant rate until the $1^{\text {st }}$ bubble appears.
14. If the bubble point doesn't appear while step one increase the temperature a little bit and use the pressure value in the step one then decrease the pressure by constant rate .

## Dew points line

1. Starting by gas sample at high temperature \& low pressure then increase the pressure by constant rate until the $1^{\text {st }}$ gas condense (dew point).
2. If the dew point doesn't appear while step one decrease the temperature a little bit and use the
3. Repeat the same procedure until the $1^{\text {st }}$ bubble appears (it appears at Tct).
4. Decrease the temperature a little
bit afterward repeat the same
procedure until get the $2^{\text {nd }}$ dew point at this point the volume of gas is $100 \%$ meanwhile the volume of condensate is $0 \%$.
5. Increasing the pressure until the volume of gas will be $0 \%$ and the volume of condensate will be $0 \%$.
6. Repeat the same procedure at step 5 \& step 6 until get the rest of dew points pressure.
7. Connect between the dews point's pressures for drawing dew point line.

## Identification of Fluid Type

Reservoir fluid type can be confirmed only by observation in the laboratory; and quick available production information usually will indicate the type of fluid in the reservoir.

| Fluid Type | API | $\begin{gathered} \hline \text { GOR } \\ \text { SCF/STB } \end{gathered}$ | Colour | $\begin{gathered} \hline \hline \text { Bo } \\ \text { BBI/STB } \end{gathered}$ | $\begin{gathered} \hline \mathbf{P i} \\ \text { Psia } \end{gathered}$ | $\begin{gathered} \hline \text { Ps } \\ \text { Psia } \end{gathered}$ | T |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ordinary black oil | 15 to 40 | 200-700 | Browndark green |  | Undersaturated <br> If $\mathrm{Pi}>\mathrm{Pb}$ | Inside <br> The envelope | Far <br> Tc |
| Low-shrinkage crude oil | less than $35^{\circ}$ | less than $200$ | Blackdeeply colored | less than $1.2$ | Saturated <br> If $\mathrm{Pi}=\mathrm{Pb}$ |  |  |
| High-shrinkage | 45-55 ${ }^{\circ}$ | 2,000- | Greenish | less than 2 |  |  |  |

International Journal of Scientific \& Engineering Research, Volume 6, Issue 5, May-2015

| (volatile) ${ }^{\text {IS }}$ 229-5518 |  | 3,200 | to orange |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Near-critical crude oil | Around $50^{\circ}$ | excess of $3,000$ |  | 2.0 or higher | $\begin{aligned} & \text { Gas-cap } \\ & \text { If } \mathrm{Pi}<\mathrm{Pb} \end{aligned}$ |  | Nearest Tc |
| Retrograde gas-condensate | above $50^{\circ}$ | $\begin{aligned} & 8,000 \text { and } \\ & 70,000 \end{aligned}$ | water- <br> white |  |  |  | Tc-Tct |
| Near-critical gasCondensate | above $60^{\circ}$ | $\begin{aligned} & 60,000 \text { to } \\ & 100,000 \end{aligned}$ | waterwhite |  |  |  | Near Tc |
| Wet gas | -_---- | 100,000 |  |  |  |  |  |
| Dry gas |  | - | ----- | ----- |  | outside The envelope | Far <br> Tc |

## Example




## Error analyses:

## Results

7. Close the inlet flash valve and slowly open the drain valve.
8. Record the initial external pump volume reading and initial gasometer volume reading.
9. Weight the $2^{\text {nd }}$ stage tube .
10. Record zero initial gasometer volume reading for the $2^{\text {nd }}$ stage.
11. Carefully open the drain valve to drain receiver tube.
12. Record the data into the blow table.
Purpose:
The Equilibrium Flash Separator can be used to measure gas oil ratio, relative volume, residual oil gravity, and related information on bottom hole.

Test Procedure:

1. This test simulates flashing from reservoir pressure or well head to separator then stock tank.

|  |  |  |  |
| :---: | :---: | :---: | :---: |
|  | Pump cell |  |  |
|  | Pressure | Volume | Temp |
|  | psia | $C C$ | ${ }^{\circ} \mathrm{C}$ |
| Initial |  |  |  |
| Final |  |  |  |
| Difference |  |  |  |
|  |  |  |  |
|  |  |  |  |

2. Close the inlet flash valve and drain valve
3. Open regulator off valve.
4. Close bypass off valve.
5. Adjust the back pressure
regulator to desired 1 st stage separator test pressure.
6. Expand the fluid sample into the separator.

| Liquid |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| First stage sep. |  |  |  | second stage sep. |  |  |
| Pressure |  | Volume | Temp | Pressure |  | Volume |
| Temp |  |  |  |  |  |  |
| Psig | psia | CC | ${ }^{\circ} \mathrm{C}$ | Psig | psia | CC |
|  |  |  |  |  |  |  |
| ${ }^{\circ} \mathrm{C}$ |  |  |  |  |  |  |
|  |  |  |  |  |  |  |


| Gas (as meaured by Gasometer) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| First stage sep. |  |  |  |  |  |  |
| Vressure |  | Volume | Temp | Pressure |  | Volume |
| Temp |  |  |  |  |  |  |
| Psig | psia | CC | ${ }^{\circ} \mathrm{C}$ | Psig | psia | CC |
| ${ }^{\circ} \mathrm{C}$ |  |  |  |  |  |  |
|  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Difference |  |  |  |  |  |  |


|  |  |
| ---: | :--- |
|  | Atmospheric |
| glass tube wt. | Pressure |
| gm | psia |
| 81.611 | 14.23 |
| 97.117 | 14.23 |
| Difference 15.5 |  |

## STO= difference Glass tube wt (g)/ difference Liquid Volume (ml)

## Formation Volume Factor=difference pump cell volume (cc)/ difference Liquid <br> Volume (cc)

Calculated Results

| GOR |  |  |  | STO |
| :---: | :---: | :---: | :---: | :---: |
| 1st <br> Stage | 2nd <br> Stage | Total | FVF | Density |


| $c c / c c$ | $c c / c c$ | $c c / c c$ | $c c / c c$ | $g / c c^{19} 6$ |
| :--- | :--- | :--- | :--- | :--- |
|  |  |  |  |  |

## at conditions

| Pressure |  |  |  | Temperature |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Reservoir | $\begin{gathered} \text { 1st } \\ \text { Stage } \end{gathered}$ | 2nd Stage | atm. | Reservoir | $\begin{gathered} \text { 1st } \\ \text { Stage } \end{gathered}$ | 2nd Stage | atm. |
| psia | psia | psia | psia | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{C}$ |
|  |  |  |  |  |  |  |  |

## Comments:

$\qquad$
$\qquad$

## Errors:

## Error analyses:

$\qquad$
$\qquad$

## EXPERIMENT NO. 9 <br> Surface tension

Ai $m$
The tensiometer measures the surface tension at a liquid- air interface at room temperature and atmospheric pressure . Theory:

The tensiometer measures the maximum force surface tension relies on the measured of the force acting on a probe by monitoring the weight change on a toploading analytical balance. Calibration:
Using the known surface tension of the water as $72.3 \mathrm{mN} / \mathrm{m}$ at 23 C .
Measurement Procedures:

1. Turn the tensiometer and the balance on.
2. Remove the draft shield cover. tip up.
3. Fill the sample glass beaker until reach the red line.
4. Put the beaker on the balance .
5. Slid the draft shield cover back in the groove.
6. Tare the balance to get a zero reading.
7. Use the up/down switch to lower the tip down until make a contact with the liquid.
8. Raise the tip while observing the decrease in mass until the mass has begun to increase.
9. At the point where the balance showed lowest reading the measurement tip has lifted the maximum amount of the fluid.
10. Record the data and calculate the surface tension as blow.

Surface tensi on (air -water)

| Please Enter Radius of measuring Tip( mm) |  |
| :--- | :--- |
| Please Enter Maximum Balance Readring (g) |  |
| Please Enter Density ( g/ml) |  |
| Volume (cubic mm) |  |
| Z |  |
| r/k |  |
| surface Tension (mN/m= dyne/cm) |  |


| Please Enter Radius of measuring Tip( mm) |  |
| :--- | :--- |
| Please Enter Maximum Balance Readring (g) |  |
| Please Enter Density ( g/ml) |  |
| Volume (cubic mm) |  |
| Z |  |
| r/k |  |
| Surface Tension (mN/m= dyne/cm) |  |

## Comments:

$\qquad$
$\qquad$

## Errors:

## Error analyses:

$\qquad$
$\qquad$

## Errors:

$\qquad$

## Error analyses:

$$
\begin{aligned}
& \mathrm{C}=-\frac{\Delta v}{v} * \\
& \frac{1}{\Delta p}=\frac{-(v 2-v 1)}{v(p 2-p 1)}=\frac{v 1-v 2}{v(p 1-p 2)} \\
& \mathrm{C}= \\
& \mathrm{psi}^{-1}
\end{aligned}
$$

is essential in performing many reservoir engineering calculations. For a liquid phase, the compressibility is small and usually assumed to be constant. For a gas phase, the compressibility is neither small nor constant.

## Test Procedure

1-Starting by Gas sample at constant temperature
2-Record the initial pressure $P_{1}$ in psia\& initial Volume $\mathrm{V}_{1}$ in cu.ft .
3-Use Jog mode then increase the volume of the Gas sample. 4-Record the new volume \& Pressure. 5- Calculate Gas Compressibility_factor -$-$

## Gas Compressibility

Knowledge of the variability of fluid compressibility with pressure and temperature

## Results

$\qquad$
$\qquad$

## Comments:

## Errors:

## Error analyses:

## EXPERIMENT NO. 12

## Dalton's Law of Partial Pressures

The total pressure exerted by a mixture of gases is equal to the sum of the pressures exerted by its components. The pressure exerted by each of the component gases is known as its partial pressure.



Dalton's law sometimes is called the law of additive pressures. Consider a mixture containing nA moles of component $\mathrm{A}, \mathrm{nB}$ moles of component $\mathrm{B}, \mathrm{nC}$ moles of component C , and so on. The partial pressure exerted by each

$$
P_{A}=n_{A} \frac{R T}{V}, P_{B}=n_{B}
$$

$$
y_{j}=\frac{P_{j}}{P}=\frac{n_{j}}{n}
$$

where yj is defined as the mole fraction of the jth component in the gas mixture. Therefore, the partial pressure of a component of a mixture of ideal gases is

$$
\begin{gathered}
P=n_{A} \frac{R T}{V}+n_{B} \frac{R T}{V} \quad \mathbf{P j}=\mathbf{y j} \mathbf{j}^{*} \mathbf{P} \\
P=\frac{R T}{V} \sum_{j} n_{j}=
\end{gathered}
$$

The ratio of the partial pressure of component Pj , to the total pressure of the mixture p is:

| Component | Mole \% | Yi | Pi=Yi*P |
| :---: | :---: | :---: | :---: |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |


|  |  |  |  |
| :--- | :--- | :--- | :--- |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
| Total |  |  |  |

HYDROGEN ION CONCENTRATION (pH):

## Comments:

| Theory |  |
| :--- | :--- |
|  | The acidity and the alkalinity of <br> the drilling fluid can be measured |
| by the concentration of the $\left(\mathrm{H}^{+}\right)$ |  |
| ion in the fluid. As for instance, |  |

## EXPERIMENT NO. 13

$\mathrm{pH}=\log$
$\left\{\frac{1}{H^{+}}\right\}=-\log \left[H^{+}\right]$

Example: If the solution is neutral then $\mathrm{H}^{+}$and $\mathrm{OH}^{-}$concentrations are the same equal to $1 \times 10^{-7}$.

1. The PH Meter: The PH meter is $\log \left(\frac{1}{1 \times 10^{-7}}\right)=-\log \left[1 \times 10^{-7}\right]=-(-7)=7$ electric device utilizing glass electrodes to measure a potential difference and indicate directly by dial reading the pH of the sample. The PH meter is the most accurate method of measuring PH
paper display certain colors in ${ }^{1963}$ certain pH ranges. It is useful, inexpensive method to determine pH in oil sample. The main disadvantage is that high concentrations of salts $(10,000$ ppm chloride) will alter the color change and cause inaccuracy.

Therefore, if the pH of a mixture drops from 7.0 to 6.0 , the number of $\left(\mathrm{H}^{+}\right)$increase ten times.
$\mathrm{pH}=$
$\log \left(\frac{1}{1 \times 10^{-7}}\right)=-\log \left[1 \times 10^{-7}\right]=-(-7)=7$

$$
=-\log 10^{-7}
$$

Methods of measuring pH in the laboratory:

1. The PH Paper: The PH paper strips have dyes absorbed into the

## The Laboratory Test:

1. Take 2 samples of crude from each tank.
2. Stir the samples for 2 minutes
3. Insert the electrode into the sample where by
(a) Use beaker to test (not steal beaker)
(b) Insert the electrode in the center
(c) Don't touch the base of the beaker

## Comments:

## Errors:

Theory
Acidity No: The amount of potassium hydroxide ( KOH ) in mg required to neutralize on e gm of Crude oil.

## Mini Acidity No >0.2 mg KOH/ gm Crude

 oil
## Aim:

Determine acidity no to know if the oil contains organic acid that may react with Alkaline or caustic flooding in order to form surfactant with the aim of reduces the interfacial tension between crude oil and water inside the reservoir hence increase productivity.

## PH

The acidity and the alkalinity of the fluid can be measured by the concentration of the $\left(\mathrm{H}^{+}\right)$ion in the fluid. As for instance, if $\mathrm{H}^{+}$is large (1 $\mathrm{x} 10^{-1}$ ), then the ( $\mathrm{OH}^{-}$) hydroxyl concentration is very low ( $1 \times 10^{-13}$ ), the solution is strongly acidic. If the $\left(\mathrm{OH}^{-}\right)$concentration is ( $1 \times 10^{-1}$ ) very high then $\left(\mathrm{H}^{+}\right)$concentration is very low then the solution is strongly alkaline. The pH of a solution is the logarithm of the reciprocal of the $\left(\mathrm{H}^{+}\right)$
concentration in grams moles per liter, ${ }^{1965}$ expresses as:

$$
\mathrm{PH}=\log \left\{\frac{1}{H^{+}}\right\}=-\log \left[H^{+}\right]
$$

Example: If the solution is neutral then $\mathrm{H}^{+}$and $\mathrm{OH}^{-}$concentrations are the same equal to $1 \times 10^{-7}$.

$$
\begin{aligned}
& \mathrm{PH}= \\
& \begin{aligned}
\log \left(\frac{1}{1 \times 10^{-7}}\right)=-\log \left[1 \times 10^{-7}\right]=-(-7)=7.00 \\
=-\log 10^{-7}
\end{aligned}
\end{aligned}
$$

Therefore, if the pH of a mixture drops from 7.0 to 6.0 , the number of $\left(\mathrm{H}^{+}\right)$ increases ten times.

Methods of measuring pH in the laboratory:

The PH Meter: The PH meter is an electric device utilizing glass electrodes to measure a potential difference and indicate directly by dial reading the pH of the sample. The PH meter is the most accurate method of measuring PH
9. Draw a line from PH axis till ${ }^{1966}$ intersects with the curve to get the KOH amount.
10. Tabulate the results here below.

## Results

## The Test Procedures:

1. Fetch oil sample from the well.
2. Pour one mg of crude oil sample into tested tube.
3. Pour $0.05 \% \mathrm{KOH}$ on the crude oil sample.
4. Stir the sample around 2 minutes
5. Insert the electrode of PH meter into the sample where by
(a) Use beaker to test (not steal beaker)
(b) Insert the electrode in the center
(c) Don't touch the base of the beaker.
6. Measure PH Value.
7. Repeat the steps from 3 till 6 using the amount $(1 \%, 1.5 \%, \ldots \ldots .5 \%)$.
8. Plot a graph between PH on Y axis versus KOH amount on x Axis.

## Comments:

$\qquad$

## Sources of errors:

$\qquad$
$\qquad$
is dispersed in the other (the continuous ${ }^{1967}$ phase)

## Error analyses:

$\qquad$

## Experiment No. 15

## Emulsion

## Stability Test

Theory


The emulsion is a mixture of two or more liquids that are normally immiscible (non mixable or unbendable). Emulsions are part of a more general class of two-phase systems of matter called colloids. Although the terms colloid and emulsion are sometimes used interchangeably, emulsion should be used when both the dispersed and the continuous phase are liquids. In an emulsion, one liquid (the dispersed phase)

## The Laboratory Test:

1. Inspect the electrode probe and cable for any evidence of damage. Ensure that the entire electrode gap is free of deposits and that the connector to the instrument is clean and dry.
2. Clean the electrode body thoroughly by wiping with a clean paper towel, be sure to clean the electrode gap.
3. Pre heat the sample to 120 F .
4. Hand stir the sample with the electrode probe for 10 sec , this will help create a uniform composition and temperature.
5. The position of the electrode probe so that it does touch the bottom or sides of the container. Be sure the electrode surfaces are completely covered by the sample.
6. Push the button to begin the voltage ramp (do not move the electrode during the voltage ramp).
7. Note the ES displayed on the readout.

## Errors:

## Error analyses:

Experiment No. 16

## Water

## Content Test

## Theory

The emulsion is a mixture of two or more liquids that are normally immiscible (non mixable or unbendable). Emulsions are part of a more general class of two-phase systems
terms colloid and emulsion are sometimes
used interchangeably, emulsion should be used when both the dispersed and the continuous phase are liquids. In an emulsion, one liquid (the dispersed phase) is dispersed in the other (the continuous phase)


## The Laboratory Test:

1. Inspect the electrode probe and cable for any evidence of damage. Ensure that the entire electrode gap is free of deposits and that the connector to the instrument is clean and dry.
2. Clean the electrode body thoroughly by wiping with a clean paper towel, be sure to clean the electrode gap.
3. Pre heat the sample to 120 F .
4. Hand stir the sample with the electrode probe for 10 sec , this will help create a uniform composition and temperature.
5. The position of the electrode probe so that it does touch the bottom or sides of the container. Be sure the electrode surfaces are completely covered by the sample.
6. Push the button to begin the voltage ramp (do not move the electrode during the voltage ramp).
7. Note the ES displayed on the readout.

## Errors:

## Error analyses:

## APPENDIX A

## Conversion Tables

| To Convert | Multiply By | To Obtain |
| :--- | :--- | :--- |
| Acres | 43,560 | Sq. feet |
| Acres | 0.00405 | Sq. kilometer |
| Acres | 4047 | Sq. meter |
| Acres | 4840 | Sq. yards |
| Acre-feet | 325,851 | Sq. feet |
| Acre-feet | 43560 | Cu. feet |
| Acre-feet | 1233.5 | m (cubed) |
| Bar | 14.5 | Lb/sq.in. |
| Bar | 1019.7 | g/cm (cubed) |
| Bar | 29.53 | inches Hg at 0 |
| Bushels (dry) | 0.03524 | degrees C |
| Centimeters | 0.03281 | msquared |
| (cm) | 0.3937 | Feet |

International Journal of Scientific \& Engineering Research, Volume 6, Issue 5, May-2015


| PPM <br> PPM <br> PPM <br> PPM <br> Percent (\%) <br> Pint <br> pt/A <br> pt/A | 0.3673 | Gal/acre-foot of water <br> lbs/million gal of water <br> $\mathrm{g} / \mathrm{kg}$ <br> liter <br> L/ha <br> oz/1000 <br> ftsquared |
| :---: | :---: | :---: |
| Pounds |  |  |
| Pounds | 0.4536 | Kilograms |
| Pounds/acre | 453.6 | Grams |
| Pounds/A | 1.12 | Kg/hectare |
| Pounds/sq.ft. | 0.02296 | $\mathrm{lb} / 1000$ ftsquared |
| Pounds/1000 | 4883 | Grams/sq.meter |
| ftsquared | 43.5597 | $\mathrm{lb} / \mathrm{A}$ |
| Pounds/yd | 0.0005937 | G/cm (cubed) |
| (cubed) | 0.12 | Kg/liter |
| Pounds/gallon | 6.9 | Kilopascals |
| PSI (lbs/sq.in.) | 0.06895 | Bar |
| PSI | 0.068046 | atm |
| PSI | 2.31 | feet head of water |
| PSI | 6.89 | kPa |
| PSI | 0.9463 | Liters |
| Quarts | 2.3385 | L/ha |
| Qt/A | 0.7346 | oz/1000 ftsquared |
| Qt/A | 0.001076 | Sq. feet |
| Sq. centimeters | 0.1550 | Sq. inches |
| Sq. centimeters | 929 | Sq. centimeters |
| Sq. feet | 0.0929 | Sq. meters |
| Sq. feet | $9.294 \times 10$ (-6) | Hectares |
| Sq. feet | 6.452 | Sq. centimeters |
| Sq. inch | 907 | kg |
| Ton (2000 lbs) | 91.44 | Centimeters |
| Yards | 0.9144 | Meters |
| Yards | 914.4 | Millimeters |
| Yards | 27 | ft (cubed) |
| yd (cubed) <br> yd (cubed) | 0.7645 | m (cubed) |

## Area Equivalents

1 acre $=43,560 \mathrm{ft}$ squared $=4840 \mathrm{yd} 2=0.4047$
hectares $=160$ rods squared $=4047 \mathrm{~m} 2=$ 0.0016 sq. mile

1 acre-inch $=102.8 \mathrm{~m} 3=27,154 \mathrm{gal}=3630 \mathrm{ft} 3$
1 hectare $($ ha) $=10,000 \mathrm{~m} 2=100$ are $=2.471$ acres $=107,639 \mathrm{ft}$ squared
1 cubic foot (ft 3 ) $=1728$ in $3=0.037$ yd $3=$ $0.02832 \mathrm{~m} 3=28,320 \mathrm{~cm} 3$

1 square foot (ft 2 ) = 144 in $2=929.03 \mathrm{~cm} 2=$
0.09290 m 2

1 square yard $(\mathrm{yd} 2)=9 \mathrm{ft} 2=0.836 \mathrm{~m} 2$
1 cubic yard $(y d 3)=27 \mathrm{ft} 3=0.765 \mathrm{~m} 3$

## Liquid Equivalents

1 ft (cubed) of water $=7.5 \mathrm{gal}=62.4 \mathrm{lbs} .=28.3$ liters
1 acre-inch of water $=27,154 \mathrm{gal}=3630 \mathrm{ft} 3$
1 liter $(\mathrm{l})=2.113$ pts. $=1000 \mathrm{ml}=1.057$ qts. $=$ $33.8 \mathrm{fl} . \mathrm{oz}$. $=0.26 \mathrm{gal}$
1 US gallon=4 qt. $=8 \mathrm{pt} .=16$ cups $=128 \mathrm{fl} . \mathrm{oz}$. $=$
8.337 lbs of water $=3.785 \mathrm{~L}=3785 \mathrm{ml}=231$ in 3
$=256 \mathrm{tbsp} .=0.1337 \mathrm{ft} 3$
1 quart $=0.9463$ liters $=2 \mathrm{pt} .=32 \mathrm{fl} . \mathrm{oz} .=4$ cups
$=64$ tablespoons (tbsp.) $=57.75$ in $3=0.25 \mathrm{gal}=$
946.4 ml

1 pint $=16 \mathrm{fl}$. oz. $=2$ cups $=473.2 \mathrm{ml}=32$ level
tablespoons $=0.125 \mathrm{gal}=0.5 \mathrm{qt}$
1 cup $=8 \mathrm{fl}$. oz. $==1 / 2 \mathrm{pt}$. $=16$ tablespoons $=$ 236.6 ml

1 tablespoon $=14.8 \mathrm{ml}=3$ teaspoons (tsp.) $=0.5$ fl.oz.
1 milliliter $(\mathrm{ml})=1 \mathrm{~cm} 3=0.34 \mathrm{fl} . \mathrm{oz}$. $=0.002$ pts
1 teaspoon $=4.93 \mathrm{ml}=0.1667 \mathrm{fl}$. oz. $=80$ drops 1 US fluid ounce $=29.57 \mathrm{ml}=2$ tablespoons $=6$ tsp. $=0.03125$ qt

## Temperature Equivalents

degrees Centigrade $=\left({ }^{\circ} \mathrm{F}-32\right) \times 5 / 9$
degrees Fahrenheit $=\left({ }^{\circ} \mathrm{Cx} 9 / 5\right)+32$

## Pressure Equivalents

1 lb per square inch $(\mathrm{PSI})=6.9$ kilopascal $(\mathrm{kPa})$
$1 \mathrm{PSI}=2.31$ feet head of water

| Units | Dyne | Lb. | Newton |
| :--- | :--- | :--- | :--- |
| Dyne | 1 | $2.248 \times 10-6$ | $10-5$ |
| Lb. | 444,823 | 1 | 4.448 |
| Newton | 100,000 | 0.2248 | 1 |

## Mixture Ratios

$1 \mathrm{mg} / \mathrm{g}=1000 \mathrm{ppm}$
$1 \mathrm{fl} . \mathrm{oz} . / \mathrm{gal}=7490 \mathrm{ppm}$
$1 \mathrm{fl} . \mathrm{oz} . / 100 \mathrm{gal}=75 \mathrm{ppm}$
$1 \mathrm{pt} / 100 \mathrm{gal}=1$ teaspoons/1gal
$1 \mathrm{qt} / 100 \mathrm{gal}=2$ tablespoons/1 gal

## Flow

$1 \mathrm{gpm}=0.134 \mathrm{ft} 3 /$ minute
$1 \mathrm{ft}(\mathrm{cubed}) / \mathrm{min} .(\mathrm{cfm})=449 \mathrm{gal} / \mathrm{hr} .(\mathrm{gph})=$ $7.481 \mathrm{gal} / \mathrm{min}$.

## Weight Equivalents

1 ton (US) $=2000 \mathrm{lb}=0.907$ metric tons $=907.2$
kg
1 metric ton $=106 \mathrm{~g}=1000 \mathrm{~kg}=2205 \mathrm{lb}$
$1 \mathrm{lb}=16 \mathrm{oz}=453.6$ grams $(\mathrm{g})=0.4536 \mathrm{~kg}$
1 oz (weight) $=28.35 \mathrm{~g}=0.0625 \mathrm{lb}$
1 gram $=1000 \mathrm{mg}=0.0353 \mathrm{oz}=0.001 \mathrm{~kg}=$ 0.002205 lb
milligrams $(\mathrm{mg})=0.001$ grams
1 kilogram $(\mathrm{kg})=1000$ grams $=35.3 \mathrm{oz}=2.205$
lbs
microgram $(\mathrm{mg})=10-6$ grams $=0.001 \mathrm{mg}$
nanogram ( ng ) $=10-9$ grams $=0.001$
micrograms (mg)
picogram = 10-12 grams
$1 \mathrm{ppm}=0.0001 \%=0.013 \mathrm{fl}$ oz in $100 \mathrm{gal}=1$
$\mathrm{mg} / \mathrm{kg}=1 \mathrm{mg} / \mathrm{L}=1 \mathrm{mg} / \mathrm{g}=0.379 \mathrm{~g}$ in 100 gal
water= $8.34 \times 10-6 \mathrm{lb} / \mathrm{gal}=1 \mathrm{~m} / \mathrm{l}$
$10 \mathrm{ppm}=0.001 \%=10 \mathrm{mg} / \mathrm{L} 100 \mathrm{ppm}=0.01 \%=$
$100 \mathrm{mg} / \mathrm{L} 1000 \mathrm{ppm}=1 \mathrm{mg} / \mathrm{g}=0.1 \%=1000 \mathrm{mg} / \mathrm{L}$
$1 \mathrm{ppb}=1 \mathrm{ug} / \mathrm{kg}$ or $1 \mathrm{ug} / \mathrm{L}$ or $1 \mathrm{ng} / \mathrm{g}$
$1 \mathrm{ppt}=1$ picogram/g
$1 \%=10,000 \mathrm{ppm}=10 \mathrm{~g} / \mathrm{L}=1 \mathrm{~g} / 100 \mathrm{ml}=10 \mathrm{~g} / \mathrm{kg}$
$=1.33 \mathrm{oz}$ by weight/gal water $=8.34 \mathrm{lbs} /$
100 gal water

## Concl usi ons

Davis, Raymond E.; Williams, John E. (2002). Modern Chemistry. Holt, Rinehart and Winston. ISBN 0-03-056537-5.
3. Guch, Ian (2003). The Complete Idiot's Guide to Chemistry. Alpha, Penguin Group Inc. ISBN 1-59257-101-8.
4. Zumdahl, Steven $S$ (1998). Chemical Principles. Houghton Mifflin Company. ISBN 0-395-83995-5.
5.Clapeyron, E (1834). "Mémoire sur la puissance motrice de la chaleur". Journal de l'École Polytechnique (in French) XIV: 153-90. Facsimile at the Bibliothèque nationale de France (pp. 153-90).

## 6.

http://www.theatlantic.com/international/ar chive/2015/03/the-hidden-consequences-
of-low-oil-prices/389156/
7. ht t p: / / web. st anf ord. edu/ cl ass/e2 97c/t rade_envi ronment/ ener gy/ hef fe ct. ht m

